## **Analytical Modeling of Natural Convection in Horizontal Annuli**

#### Peter Teertstra, M. Michael Yovanovich, J. Richard Culham

Microelectronics Heat Transfer Laboratory Department of Mechanical Engineering University of Waterloo Waterloo, Ontario, Canada

12 January, 2005



#### Outline



- Introduction and problem description
- Literature review and objectives
- Model development
- Validation
- Summary and conclusions

## **Problem Definition**

- 2D horizontal annulus
- Steady state, natural convection
- Concentric inner and outer cylinders
- Isothermal boundary conditions,  $T_i > T_o$



Geometry:

Relative boundary size

$$P_o / P_i \Longrightarrow d_o / d_i$$
 (spheres)

Effective gap spacing

$$\delta_e \Rightarrow (d_o - d_i)/2$$
 (spheres)

Shape, orientation



## **Parameter Definitions**



 Total heat transfer rate non-dimensionalized by Nusselt number

$$Nu = \frac{Q \ell}{k P_i (T_i - T_o)}$$

- $P_i$  selected as characteristic length:
  - For  $P_o / P_i \rightarrow \infty$  limit, scale length related to inner body dimensions only
  - Similar results for similar body shapes, orientations

$$Nu_{P_i} = \frac{Q}{k\left(T_i - T_o\right)}$$



## **Parameter Definitions**



Dimensionless conduction shape factor

 $\lim_{Ra \ll Ra_{cr}} Nu_{P_i} = S_{P_i}^*$ 

• Effective conductivity

$$\frac{k_{eff}}{k} = \frac{Nu_{P_i}}{S_{P_i}^*}, \qquad \frac{k_{eff}}{k} \ge 1$$

• Rayleigh number

$$Ra_{P_i} = \frac{g\beta(T_i - T_o)(P_i)^3}{\upsilon\alpha}$$



## **Literature Review - Data**



#### **Experimental and Numerical Studies**

- Concentric spherical enclosures
  - Over 20 publications with average heat transfer data
  - Most experimental data for high Rayleigh number, boundary layer flow
  - All other data from numerical simulations
- Other enclosure geometries
  - Numerical data for circular, polygonal, rhombic, elliptical cylinders

• Correlations of experimental, numerical data

- Valid for limited ranges of Rayleigh number
- Geometry-dependent



## **Literature Review - Models**



- Analytical models available for concentric, eccentric circular annulus
  - Raithby & Hollands<sup>28</sup>
  - Kuehn and Goldstein<sup>29</sup>
- Boyd<sup>30</sup> presents general correlation procedure for 2D annulus with arbitrarily-shaped boundaries
  - Requires correlation coefficient values from empirical data
  - Difficult to implement for non-standard boundary shapes

## **Objectives**



- Analytical modeling of natural convection in horizontal annulus
  - Full range of  $Ra_{P_i}$  from conduction to convection
  - Applicable to wide range of geometries
    - Inner and outer boundary shapes and orientation
    - Relative boundary sizes
  - Physically-based analysis
- Validate model using experimental, numerical data from the literature
  - Circular annulus
  - Annuli with different inner, outer boundary shapes



#### **Model Development**

• Assume linear superposition of diffusive, convective limits

University of

$$Nu_{P_i} = S_{P_i}^* + Nu_{\rm conv}$$

• Kuehn and Goldstein<sup>8,9</sup> data for circular annulus



### **Model Development**



 General model based on Churchill and Usagi<sup>33</sup> composite solution technique

$$Nu_{P_i} = S_{P_i}^* + \left[ \left( \frac{1}{Nu_{tr}} \right)^n + \left( \frac{1}{Nu_{bl}} \right)^n \right]^{-1/n}$$

Combination of three asymptotic solutions

 $S_{P}^{*} =$ conduction shape factor

 $Nu_{tr}$  = transition flow convection

 $Nu_{bl}$  = laminar boundary layer convection

• Combination parameter *n* determined from validation with numerical, experimental data

## **Conduction Shape Factor**

- Correlations, models, from handbooks
- Numerical simulations
- Approximate method from equivalent circular annulus

 $S_{P_i}^* = \frac{2\pi}{\ln(d_1/d_2)}$ 

- Effective diameter ratio  $\left(\frac{d_o}{d_i}\right)_e \Rightarrow$  Inner perimeter  $d_i = P_i/\pi$ Enclosed area  $d_o = \sqrt{\frac{4A}{\pi} + \frac{P_i^2}{\pi^2}}$
- Dimensionless conduction shape factor

$$S_{P_i}^* = \frac{2\sqrt{\pi}}{\ln\sqrt{4\pi\left(A/P_i^2\right) + 1}}$$



# **Boundary Layer Convection**

- Assumptions
  - Laminar flow
  - $T_b$  uniform

- $T_i \xrightarrow{} R_i \xrightarrow{} T_b \xrightarrow{} R_o \xrightarrow{} T_o$
- Non-intersecting boundary layers
- Series combination of resistances

$$R = R_i + R_o \qquad R_i = \frac{T_i - T_b}{Q} \qquad R_o = \frac{T_b - T_o}{Q}$$

Non-dimensionalize using Nusselt number

$$\begin{split} R_i = & \frac{T_i - T_b}{Q} \qquad R_o = \frac{T_b - T_o}{Q} \qquad Nu_{bl} = \frac{1}{k(R_i + R_o)} = \frac{Nu_i}{1 + 1/\phi} \\ & \phi = \frac{T_i - T_b}{T_b - T_o} = \frac{R_i}{R_o} = \frac{Nu_o}{Nu_i} \end{split}$$





# **Boundary Layer Convection**



University of

Convection modeled using Yovanovich<sup>31</sup> and Jafarpur<sup>36</sup>

$$Nu_{\sqrt{A}} = F(\Pr) G_{\sqrt{A}} Ra_{\sqrt{A}}^{1/4}$$

Laminar boundary layer convection asymptote

$$Nu_{bl} = \frac{Nu_{i}}{1+1/\phi} = \frac{F(\Pr)G_{P_{i}}Ra_{P_{i}}^{1/4}}{(1+1/\phi)^{5/4}}$$

$$Nu_{bl} = \frac{F(\Pr)G_{P_{i}}Ra_{P_{i}}^{1/4}}{\left[1+(P_{i}/P_{o})^{3/5}(G_{P_{i}}/G_{P_{i}})^{4/5}\right]^{5/4}}$$

$$Nu_{bl} = \frac{(1.028)F(\Pr)Ra_{P_{i}}^{1/4}}{\left[1+(d_{i}/d_{o})^{3/5}\right]^{5/4}} \quad \text{(circular annulus)}$$

## **Transition Flow**

- Boundary layers merge when  $Ra < Ra_{cr}$
- Model as equivalent circular annulus •
- Three distinct regions are formed
- Central region
  - Radial conduction
  - Buoyancy induced flow
- For narrow gap spacing,  $\delta_{\rho} \ll r_i$ , temperature, velocity in central region

$$T - T_b = -\frac{y}{\delta_e/2} (T_i - T_b), \quad T_b = \frac{T_i + T_o}{2}$$
$$u = \frac{g_e \beta}{12\upsilon} (T_i - T_o) \left(\frac{\delta_e}{2}\right)^2 \left[ \left(\frac{y}{\delta_e/2}\right)^3 - \frac{y}{\delta_e/2} \right]$$



## **Transition Flow**

• Enthalpy balance in top-end and bottom-end regions

$$Q_{i,o} = \frac{\rho c_{p} g_{e} \beta (T_{i} - T_{o})^{2} \delta_{e}^{3}}{720 \nu}$$

• Transition flow asymptote

$$Nu_{tr} = \frac{1}{90 \pi} \frac{(\delta_{e}/P_{i})^{3}}{(1 + P_{o}/P_{i})} Ra_{P_{i}}$$
$$Nu_{tr} = \frac{1}{720 \pi^{4}} \frac{(d_{o}/d_{i}-1)^{3}}{(1 + d_{o}/d_{i})} Ra_{P_{i}}$$
(circular annulus)























## Summary



- Analytical study of natural convection heat transfer for isothermal, horizontal annuli
- Model developed based on combination of analytic, asymptotic relationships
  - Diffusive limit
  - Laminar boundary layer convection
  - Transition flow convection
- Validated using previous data for similar, different inner and outer cylinder shapes
- 6 9% RMS difference between model and data

