



# **Microelectronics Cooling**

## **“An Overview”**

**J. Richard Culham**

Microelectronics Heat Transfer Laboratory  
Department of Mechanical Engineering  
University of Waterloo

# Outline

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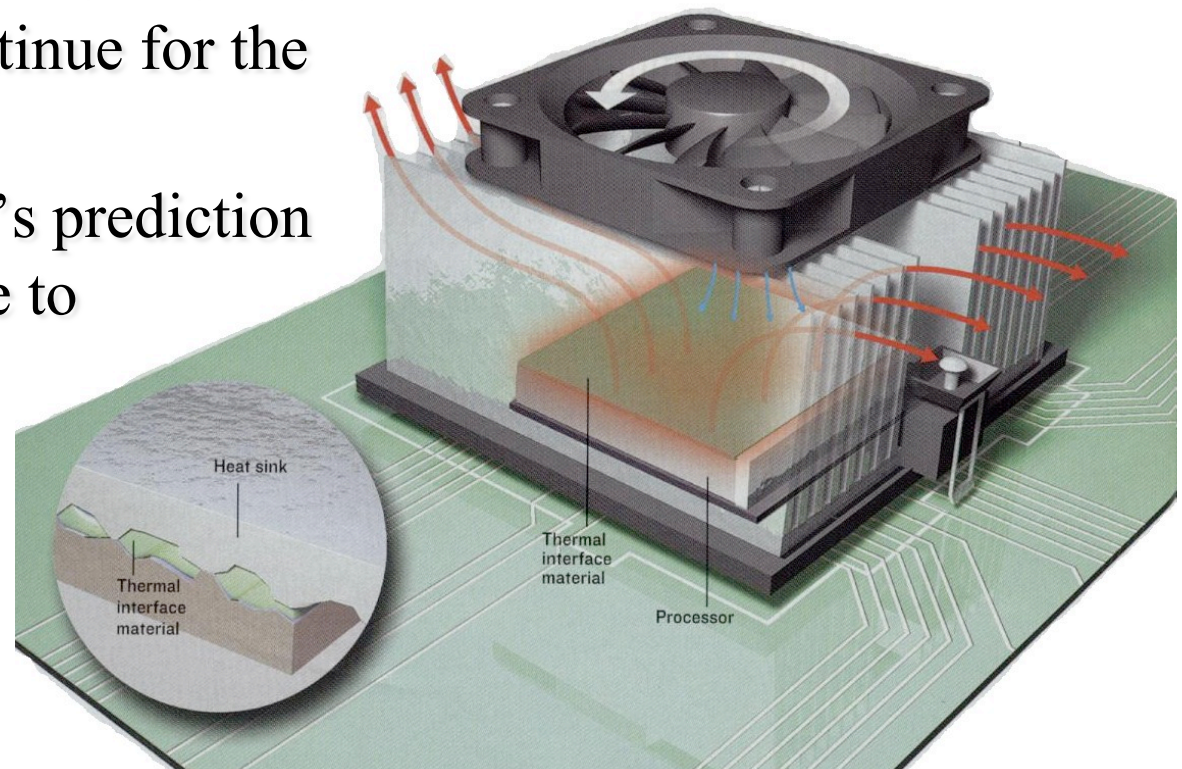


- Motivation
- Thermal Networks
  - Bulk properties
  - Spreading/constriction
  - Boundary heat transfer
  - Joint/interface heat transfer

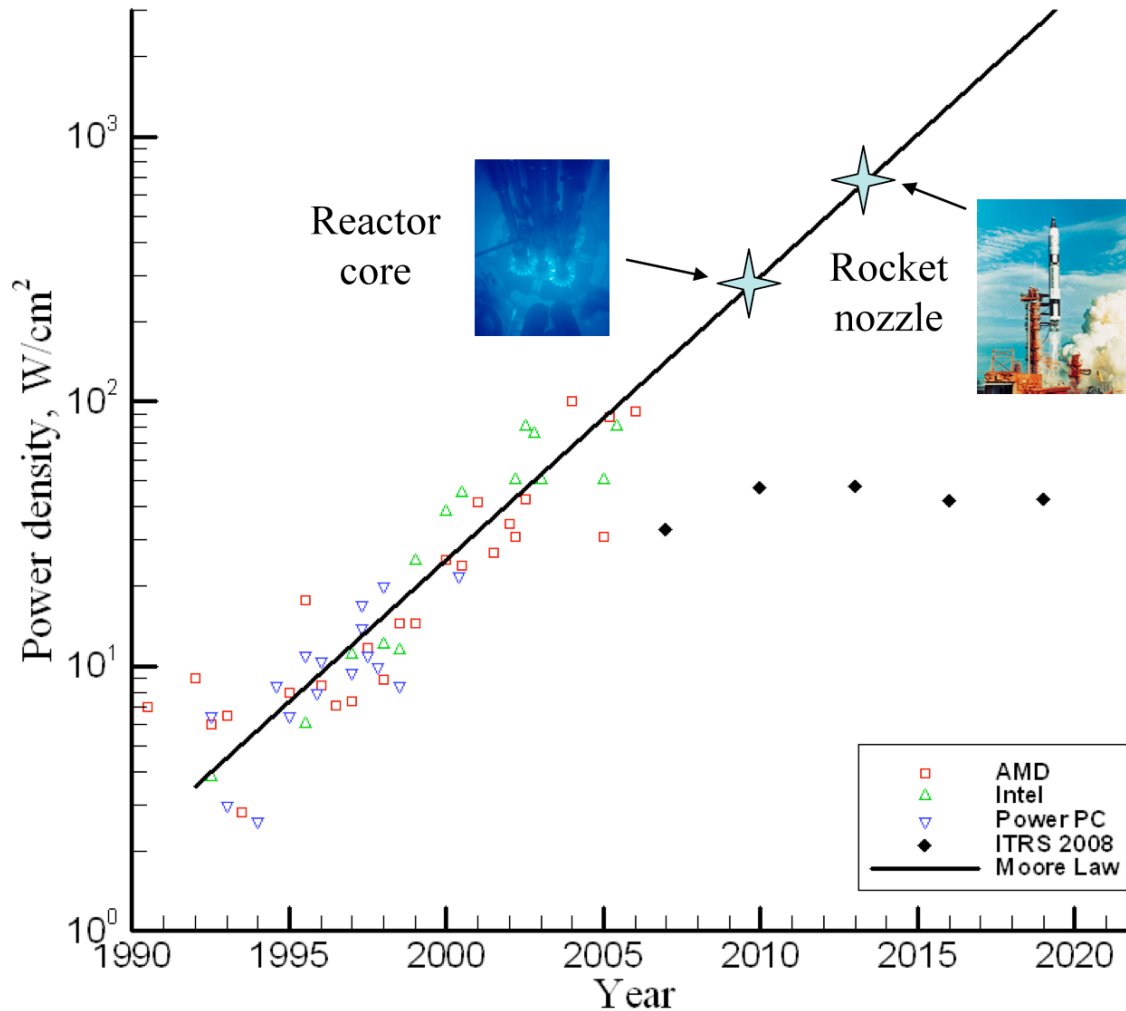
# Motivation



- Heat loads typically follow transistor density
- 1965: Gordon Moore observed that transistor density on ICs was doubling every 18 months and predicted it would continue for the foreseeable future
- After 45 years, Moore's prediction is beginning to fail due to thermal management issues

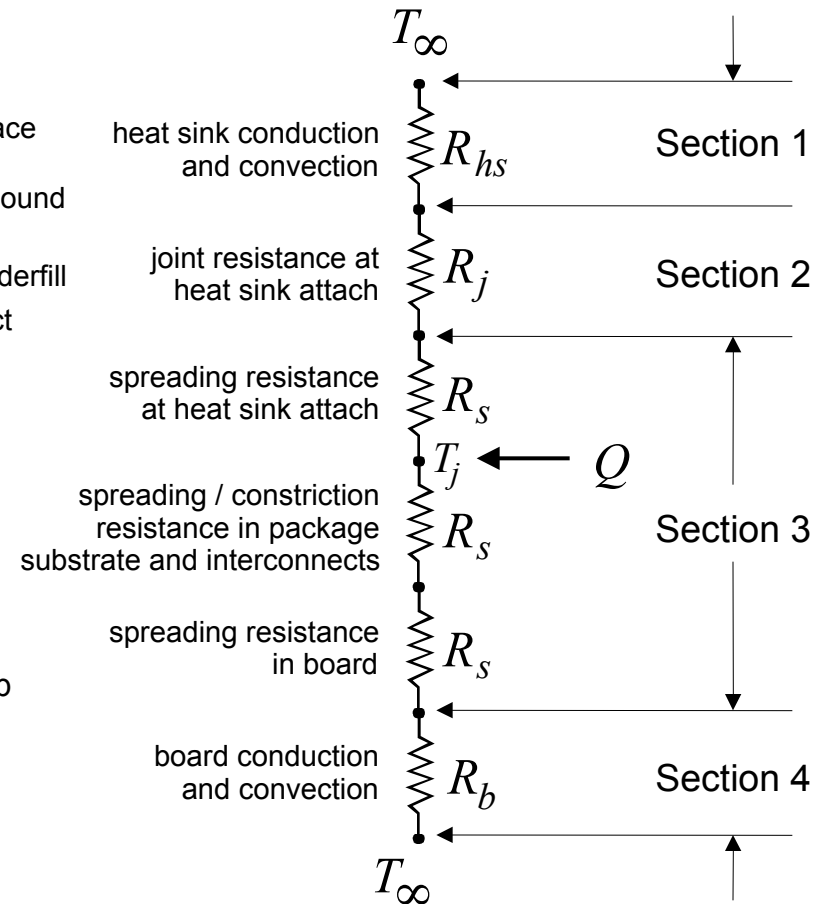
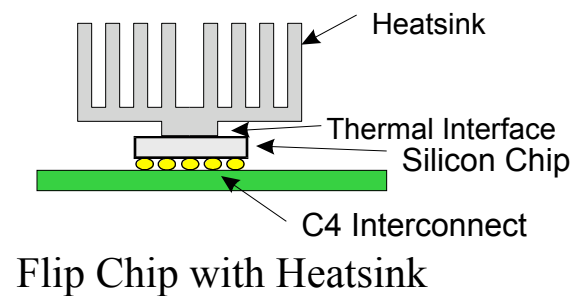
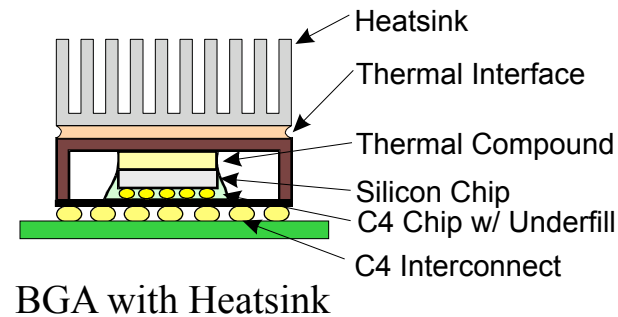
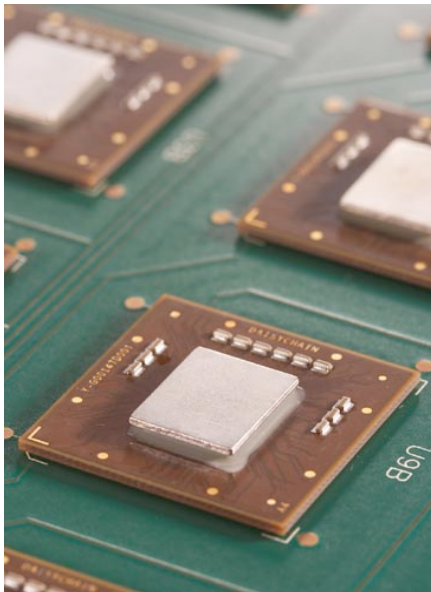


# Cooling Limits





# Thermal Resistance Network

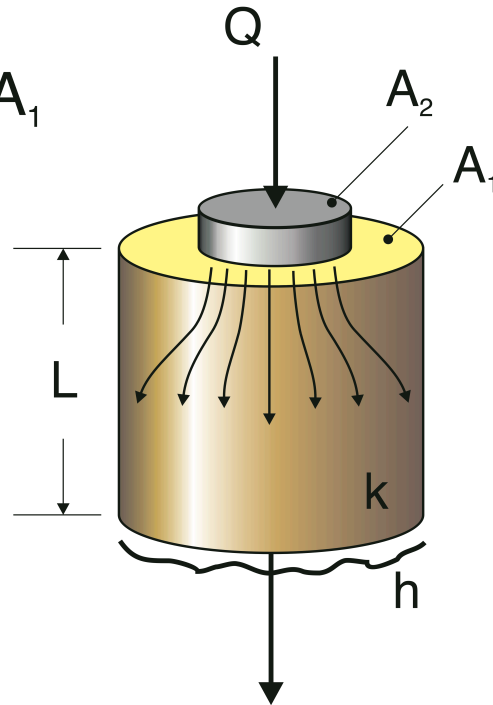


# Component Resistances



## Material

$$R_{\text{bulk}} = L/kA_1$$



## Spreading

$$R_s = \frac{\psi}{\sqrt{\pi} k A_1}$$

where  $\psi = f(A_1/A_2, L, h, k)$

## Joint

$R_j = 1/(h_j A_2)$ , where

$$h_j = h_c + h_g$$

$$\left\{ \frac{h_c \sigma}{m k} \right\} = 1.25 \left\{ \frac{P}{H} \right\}^{0.95}$$

$$h_g = \frac{k_g}{Y + M}$$

## Boundary

$$R_{\text{bound}} = \frac{1}{h A_1}$$

# Effects of Scale



Case 1:  $k=20$  W/mK,  $t=2$  mm,  $r_1=20$  mm,  $r_2= 2$  mm,  $h = 20$  W/m<sup>2</sup>K

scale by factor of 0.01



Case 2:  $k=20$  W/mK,  $t=0.02$  mm,  $r_1= 0.2$  mm,  $r_2= 0.02$  mm,  $h = 20$  W/m<sup>2</sup>K

$^{\circ}\text{C}/\text{W}$	Order	Case 1	Case 2
$R_{\text{bulk}}$	$L^{-1}$	0.08	8
$R_{\text{contact}}$	$L^{-2}$	14	$1.4 \times 10^5$
$R_{\text{spreading}}$	$L^{-1}(L^{-2})$	9.2	922 ( $9 \times 10^4$ )
$R_{\text{boundary}}$	$L^{-2}$	40	$4 \times 10^5$

# Bulk Properties

- Effective conductivity calculator based on Fourier series analysis
- Up to 20 layers, pre-programmed material properties available
- Calculated  $k$  effective based on relative source size, position and edge conditions

<http://mhtlab.uwaterloo.ca/RScalculators.html>

Effective Conductivity (ID:9) - Microsoft Internet Explorer

## Effective Conductivity of Multilayered Substrates

Substrate		
Length (mm)	$L$	100
Width (mm)	$W$	100
Convective Coefficients ( $W/m^2K$ )	$h_{top}$	5
	$h_{bot}$	5
Number of Layers		3

Layer #	Composition	Conductivity $k$ (W/mK)	Thickness $t$ (mm)	Edge Conductance $h_{edge}$ ( $W/m^2K$ )
1	Other	10	1	0
2	Other	10	1	0
3	Other	10	1	0

Heat Source		
Length (mm)	$L_s$	40
Width (mm)	$W_s$	40
Position (mm) (lower-left corner)	$X$	30
	$Y$	30
Power (W)	$Q$	3

# Spreading Resistance



- General series solution for rectangular, multi-layered flux tubes: “*Influence of Geometry and Edge Cooling on Thermal Spreading Resistance,*” Muzychka, Y.S., Yovanovich, M.M. and Culham, J.R., *AIAA Journal of Thermophysics and Heat Transfer*, Vol. 20, No. 2, April-June, 2006, pp. 247-255.

*Journal of Thermophysics and Heat Transfer*, Vol. 20, No. 2, April-June, 2006, pp. 247-255.

Spreading Resistance of Rectangular Source on Rectangular Disk with Edge Cooling

Source Dimensions		Substrate Dimensions	
2a [mm]	2b [mm]	2c [mm]	2d [mm]
<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>

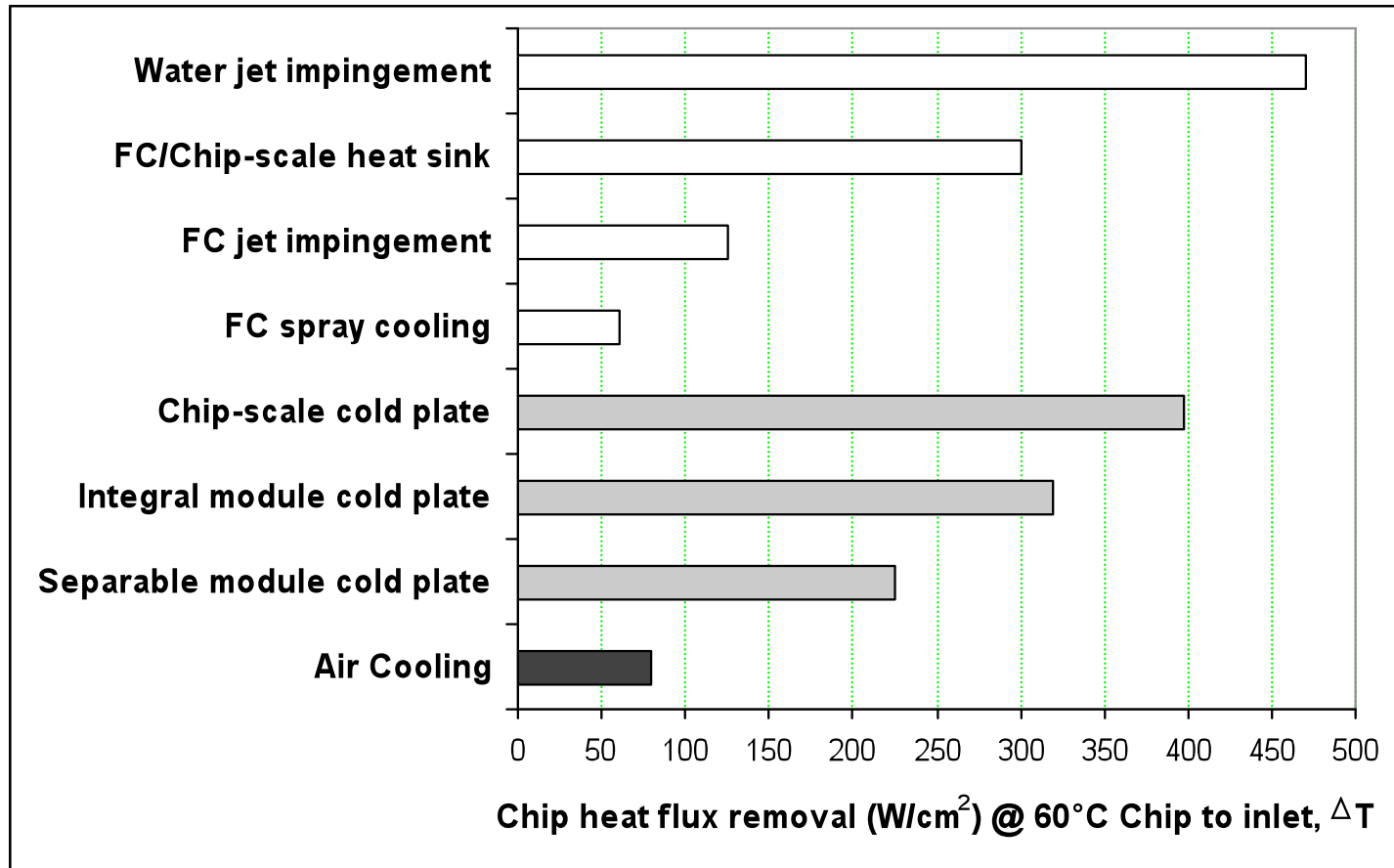
Side Film Coefficient $h_s$ [W/m <sup>2</sup> K]	Thickness $t$ [mm]
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Number of Terms $N$	End Film Coefficient $h_e$ [W/m <sup>2</sup> K]
<input type="text"/>	<input type="text"/>
Thermal Conductivity $k$ [W/m K]	
<input type="text"/>	

Number of Digits

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- Circular and rectangular substrates
- Single and multi-layers
- Finite, semi-infinite and infinite flux tubes
- Circular, strip and rectangular sources
- Isoflux, Parabolic, Equivalent Isothermal sources
- Edge cooling

# Cooling Potential

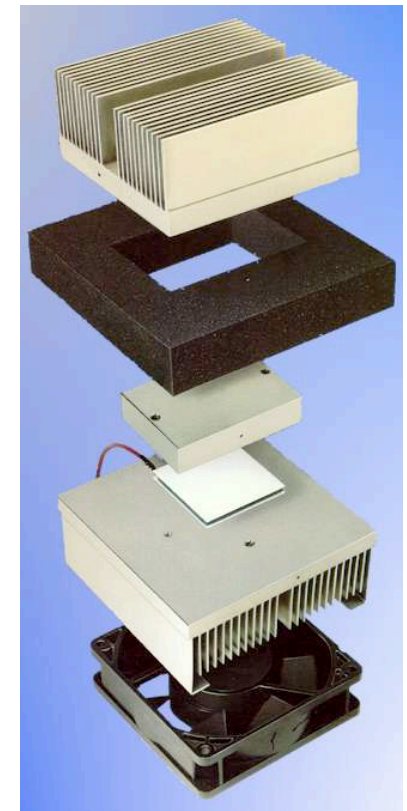
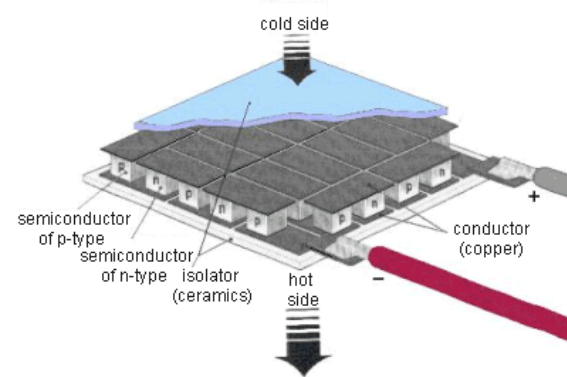




# Boundary Heat Transfer



- Extended surfaces
  - Heat sinks: natural convection, forced convection
  - Cold plates: single phase liquid
- Two phase
  - Micro-refrigeration
  - Vapor chambers
  - Heat pipes
  - Hybrid systems
- Peltier devices



# Heat Sinks

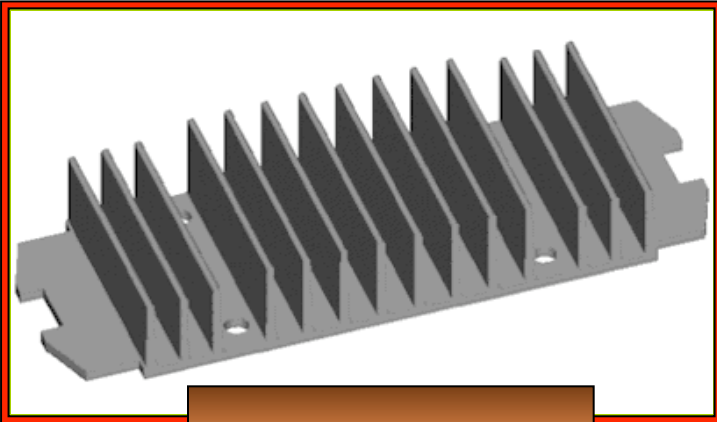
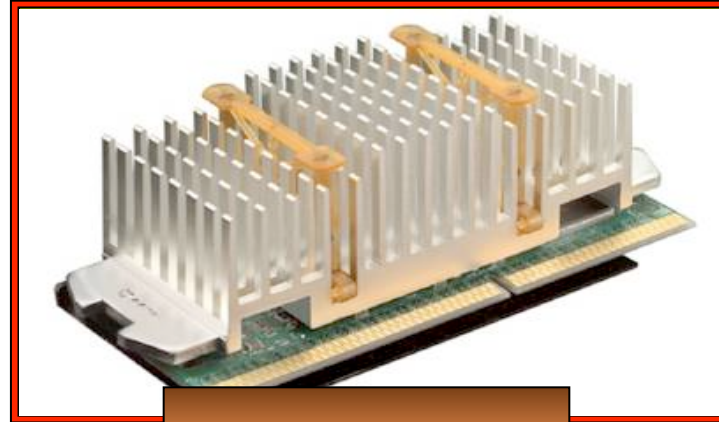


Plate Fin H.S.

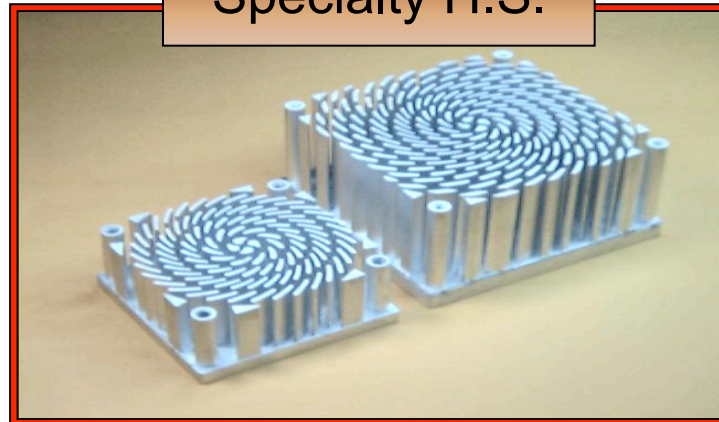


Pin Fin H.S.

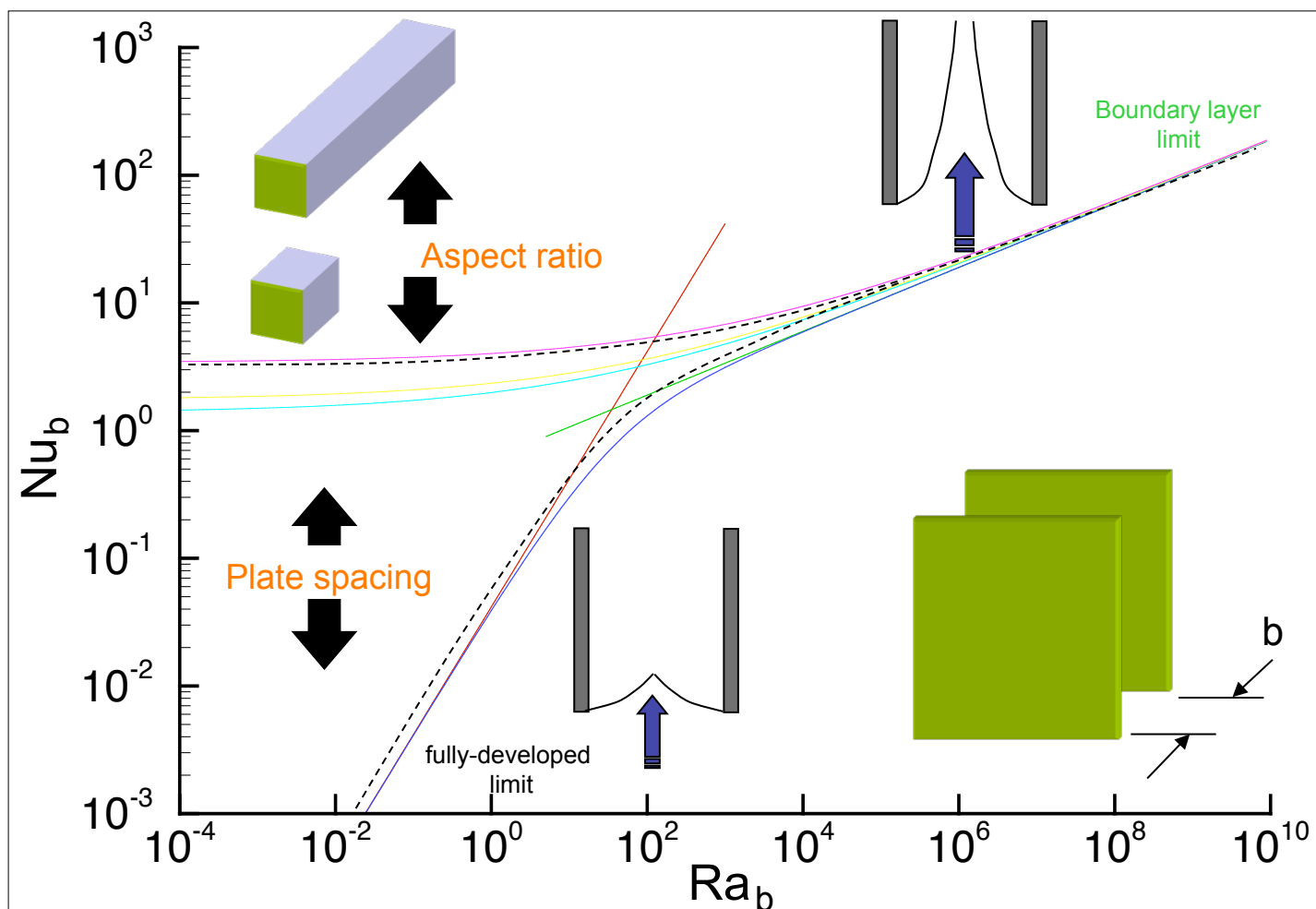
Radial Fin H.S.



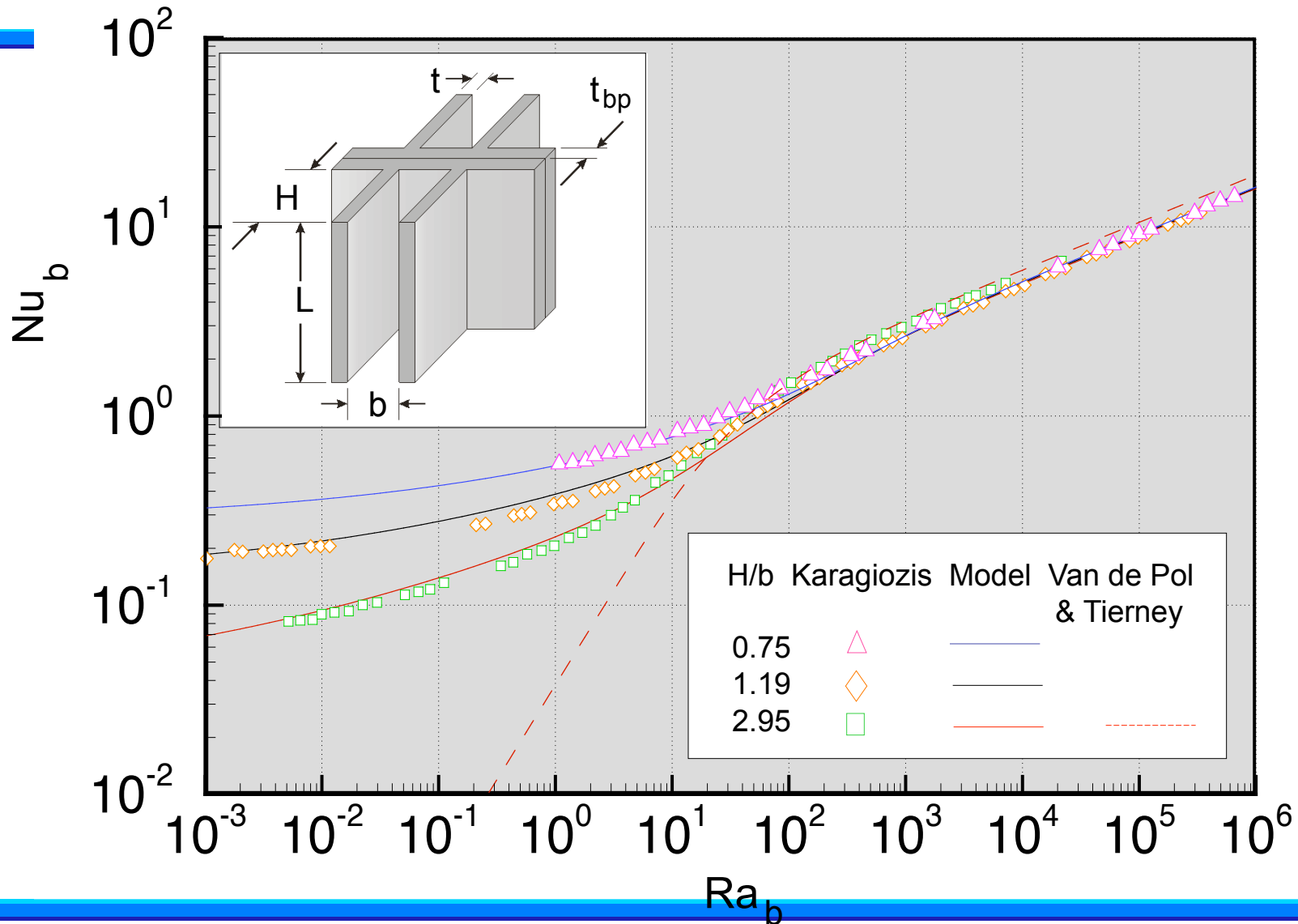
Specialty H.S.



# Modeling of Natural Convection



# Model Validation



# Heat Sink Models



## Entropy generation minimization model

- select maximum working volume
- assign values to fixed parameters
- click calculate to determine optimum value for free parameters
- can be up to 9 free parameters
- determines true, simultaneous optimum value for all free parameters
- solution procedure is applicable for any thermodynamic system

Heat Sink Optimization: Plate Fin

Instructions Background Input/Output References

**Optimize Value**

**Base Plate**

Length  100 mm

Width  100 mm

Thickness  10 mm

**Fin**

Height  50 mm

Thickness  2 mm

Number

**Thermal Conductivity**

Fin  180 W/mK

Baseplate  180 W/mK

Approach Velocity  2 m/s

**Maximum Dimensions**

L  mm

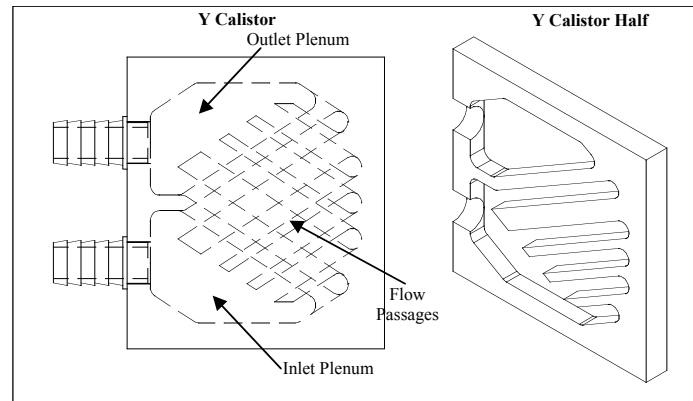
W  mm

H  mm

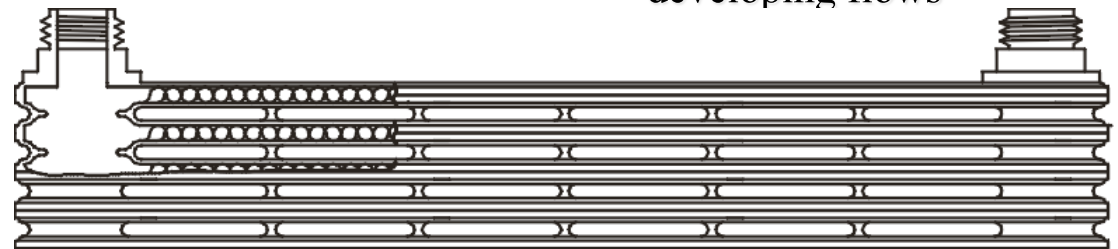
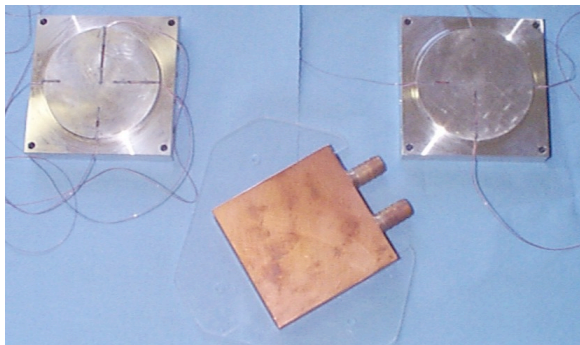
Calculate Reset



# Single Phase, Liquid Cooling

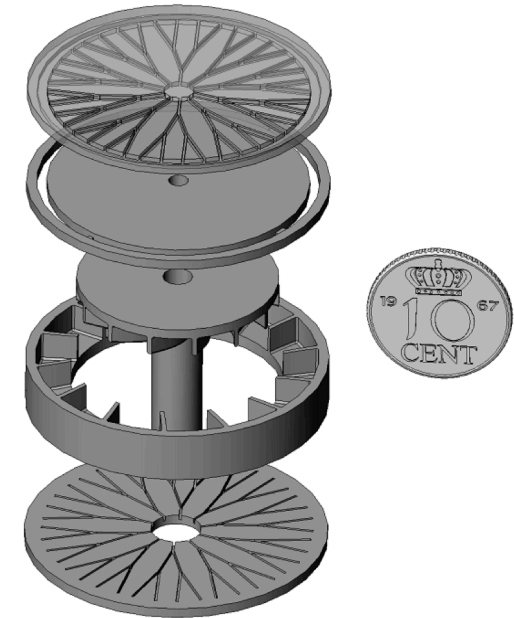
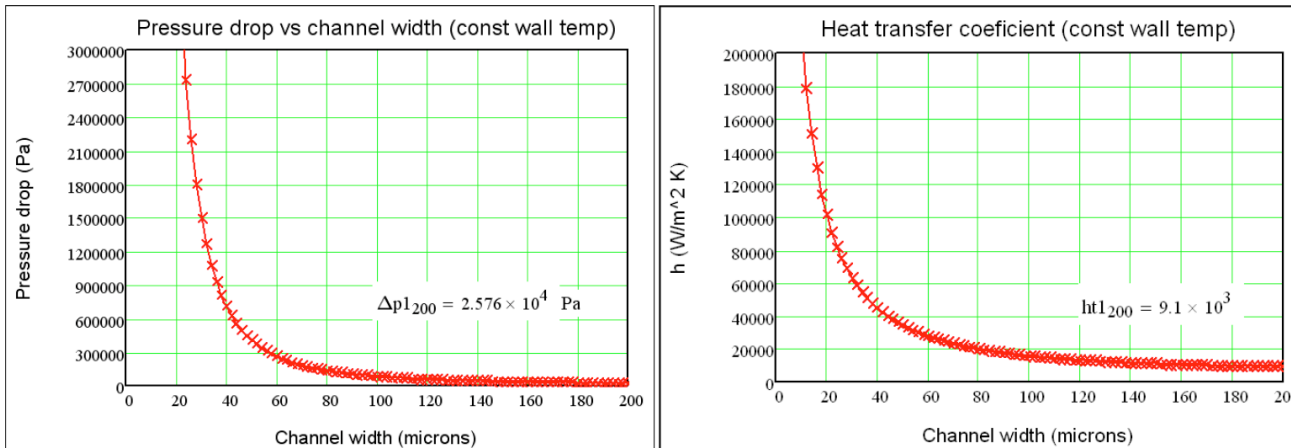


- Compact cold plates for high heat flux applications
- Modeling and testing of:
  - Fully developed flow
  - Thermally developing flow
  - Simultaneously developing flows

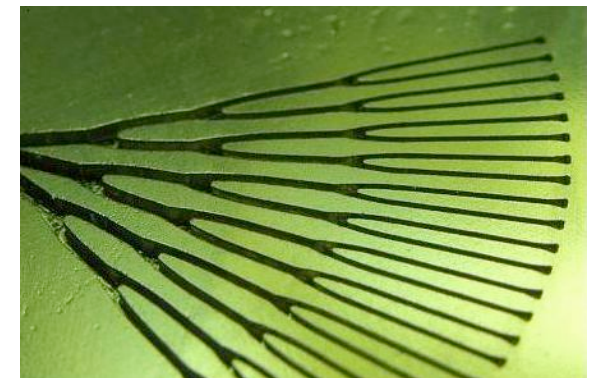
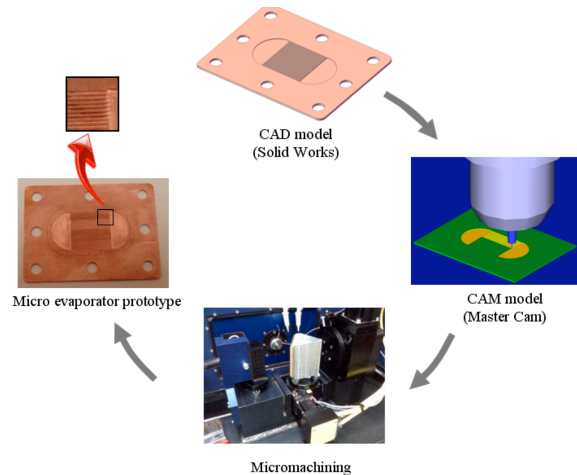




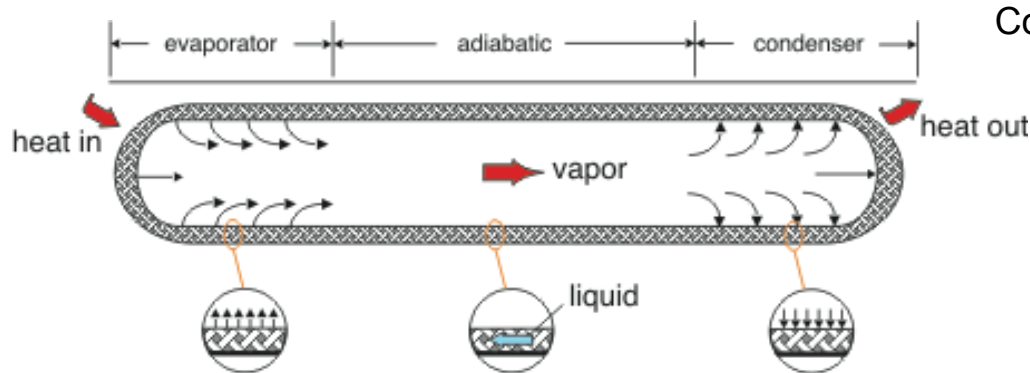
# Micro-refrigeration



**Figure 4-5: MHE Pressure Drop and Heat Transfer Coefficient vs. Channel Width (Channel length 15 mm, depth 200 mm, flow  $3.39 \times 10^{-3}$  kg/s,  $T_{wall} = 59$  °C)**



# Heat Pipes



Conventional Heat Pipe

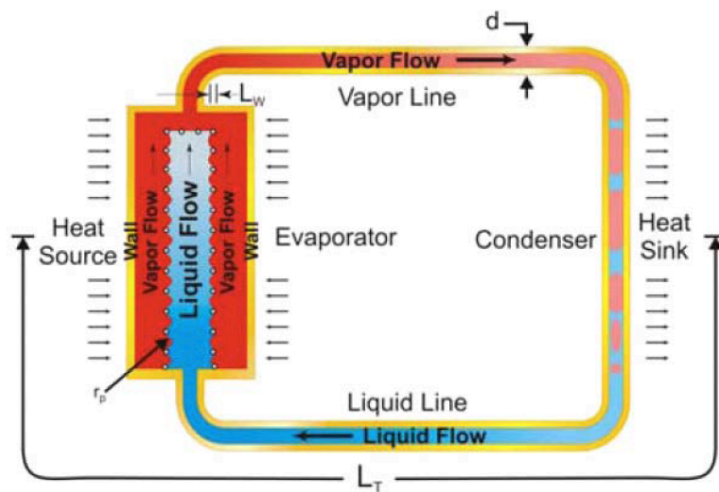
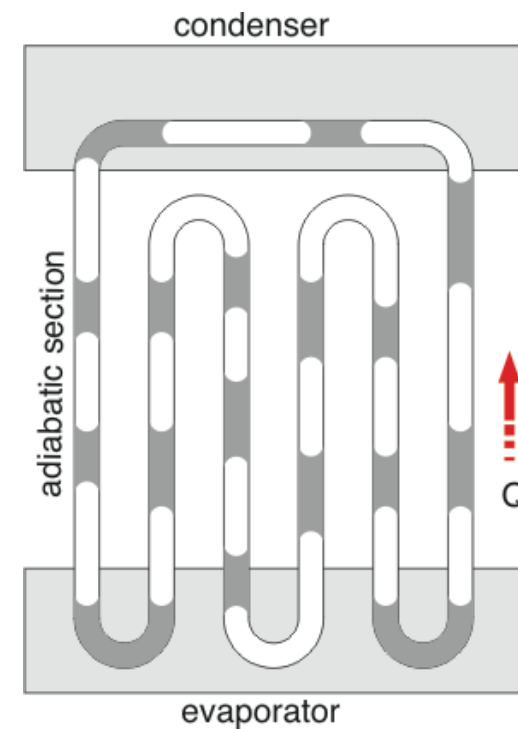


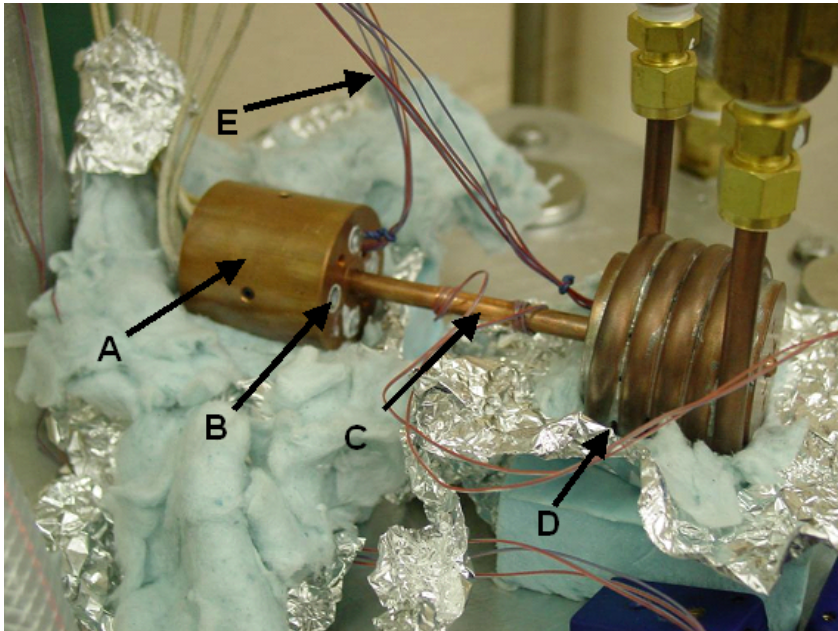
Figure 8: Typical Loop Heat Pipe

(Source: <http://www.swales.com>)

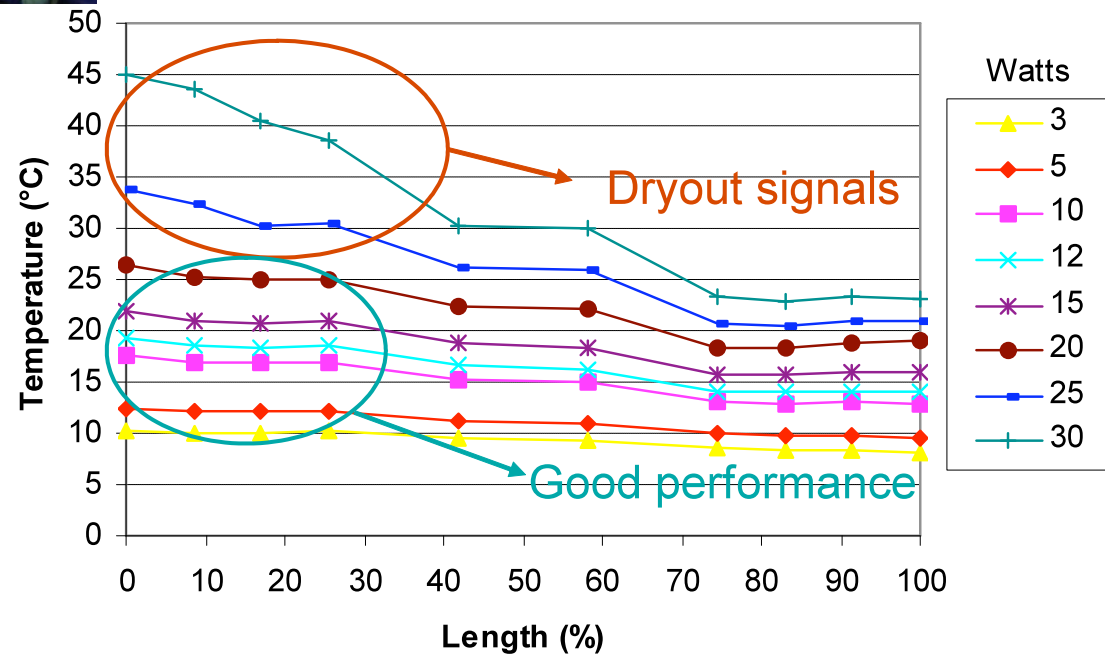


Pulsating Heat Pipe

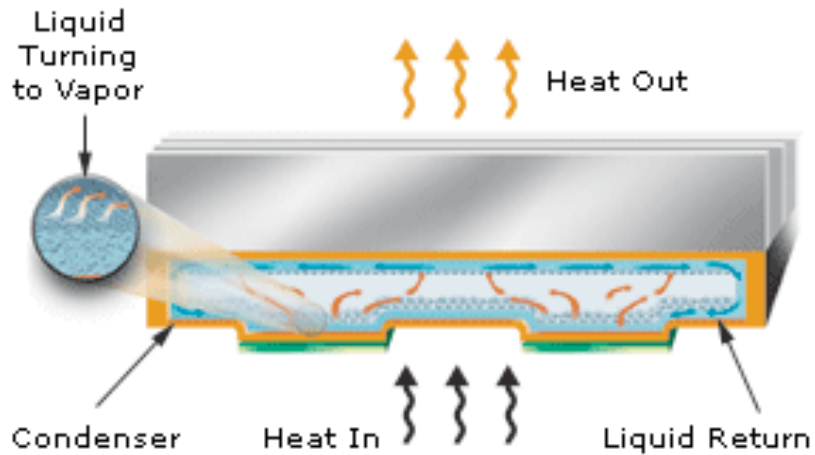
# Heat Pipes



Temperature Profile vs HP Length  
 D=5 mm, L= 150 mm (Coolant 5°C)

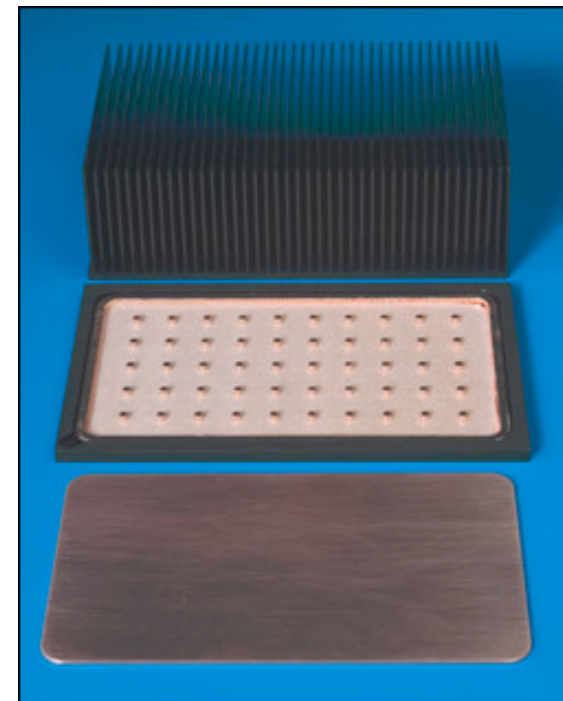
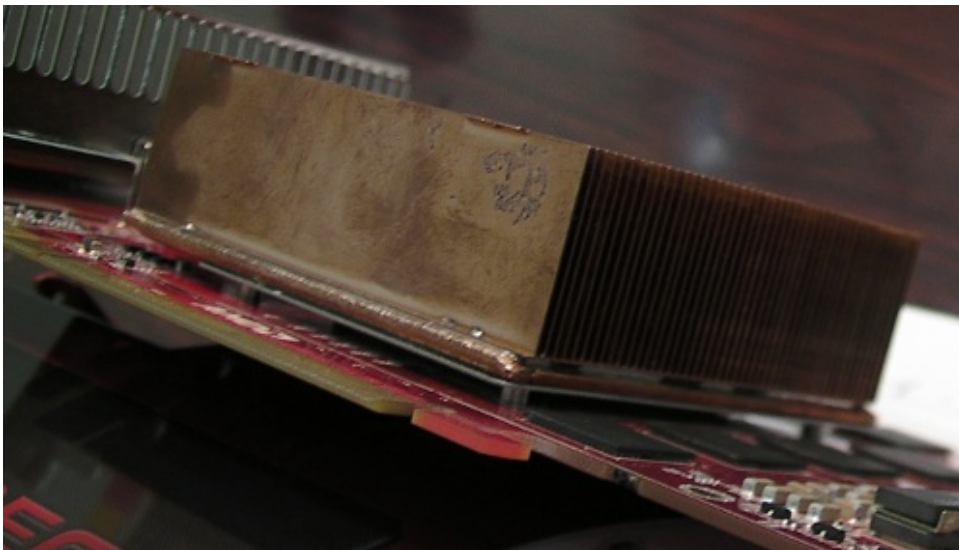


# Vapor Chambers



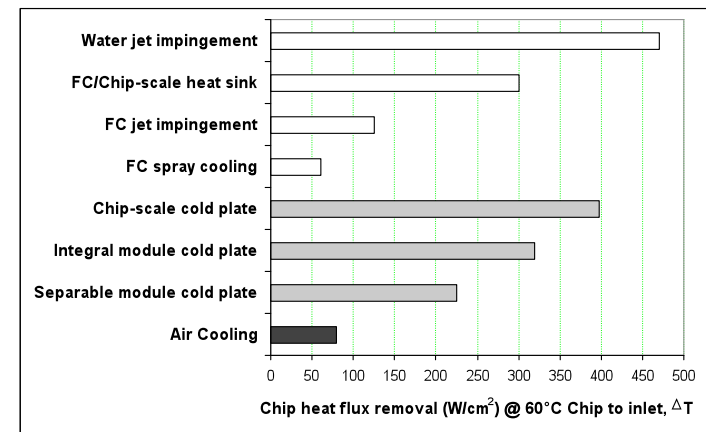
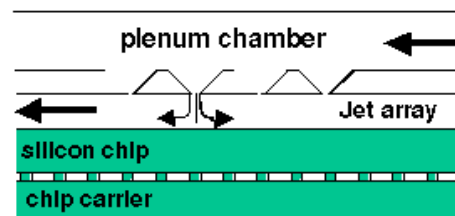
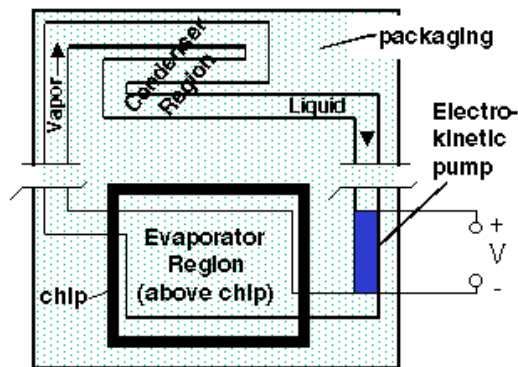
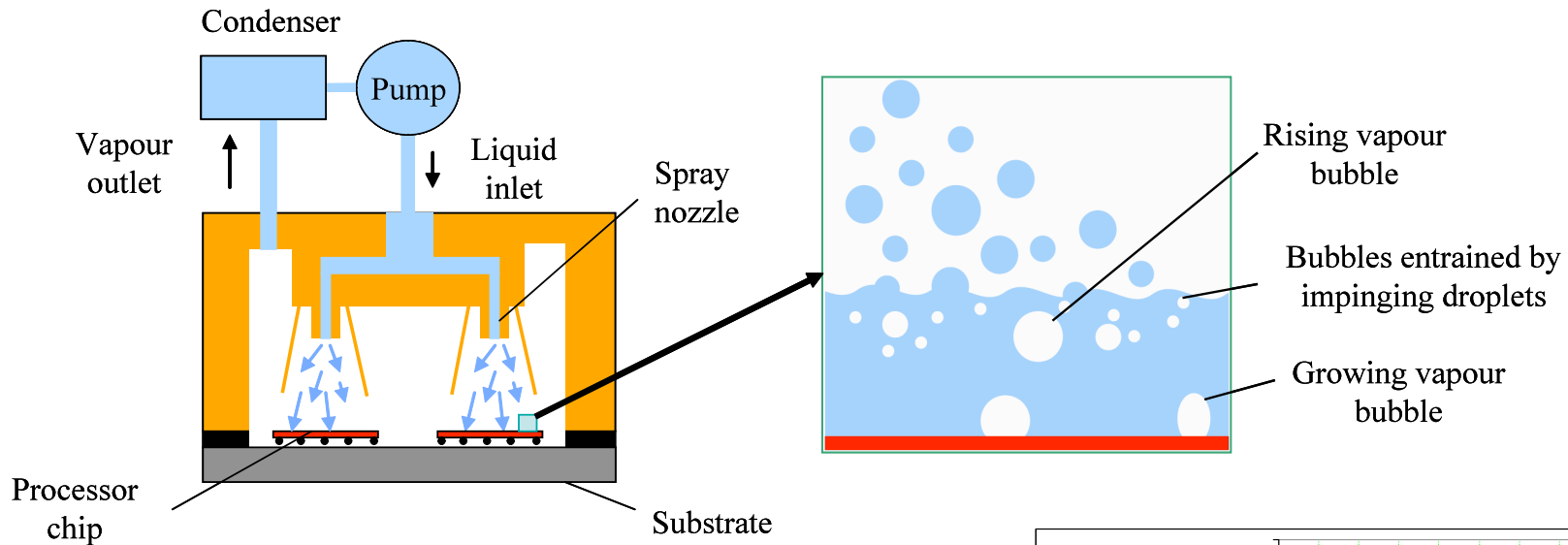
Illustrations courtesy of Thermacore and Advance Cooling Technologies

- <http://www.1-act.com/>
- <http://www.thermacore.com/>

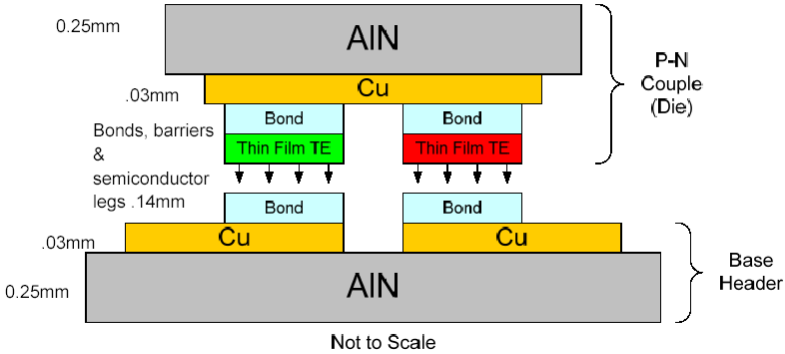
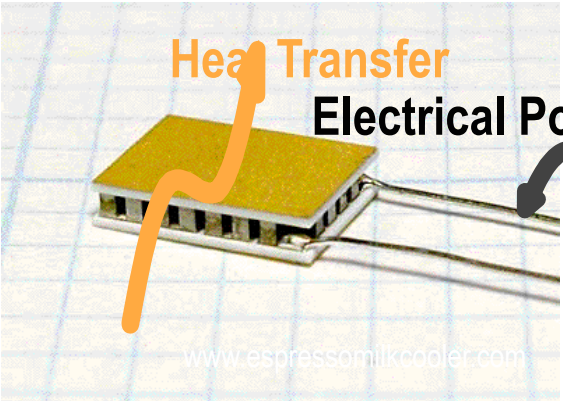




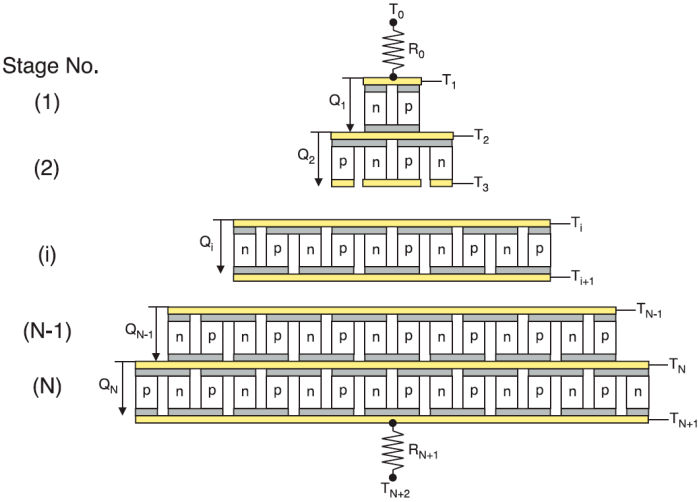
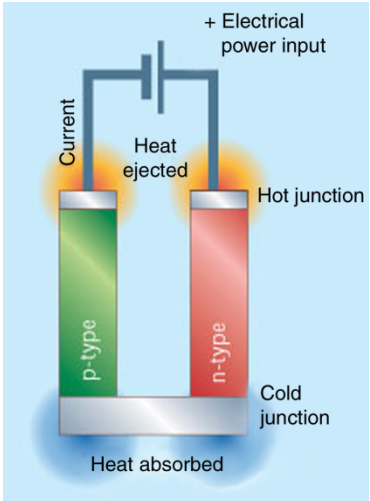
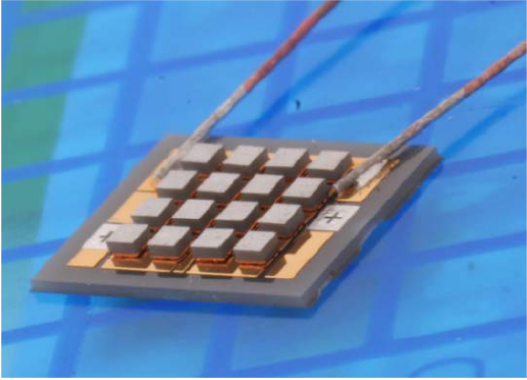
# Jet Impingement



# Peltier Devices

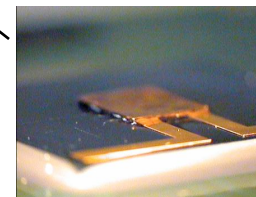
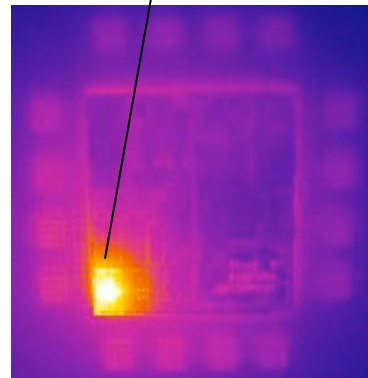
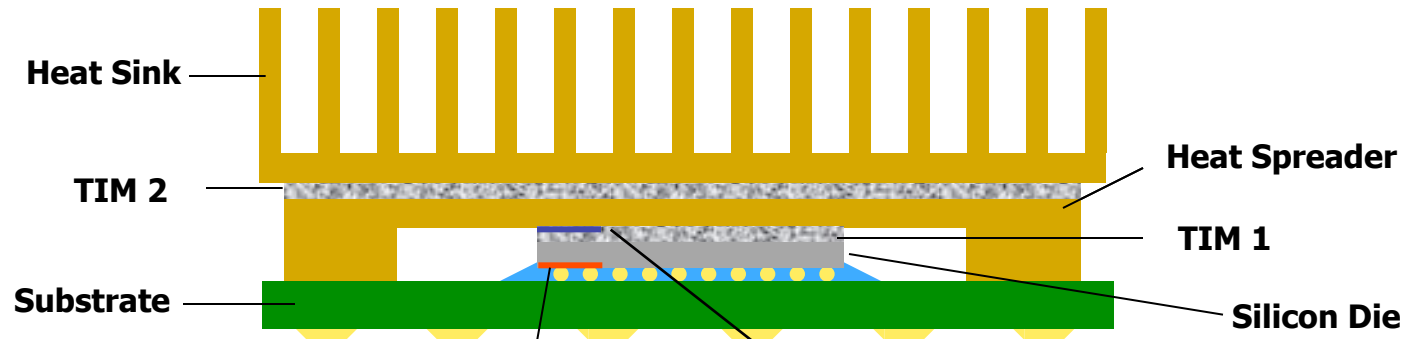


- electric current driven through a Bismuth-Telluride junction
- heat absorbed at the cold junction and released at the hot junction





# Embedded Semiconductor Cooling

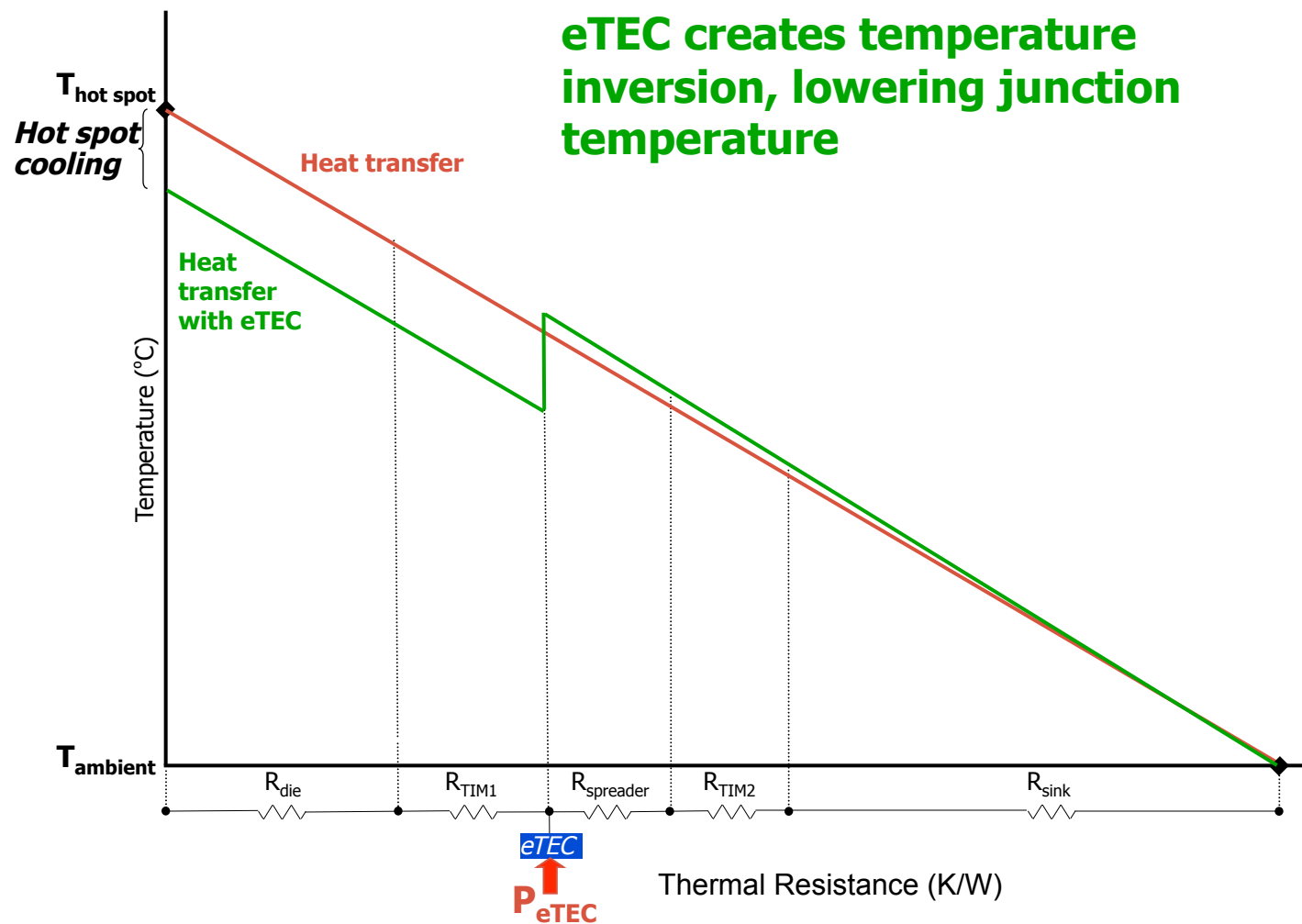


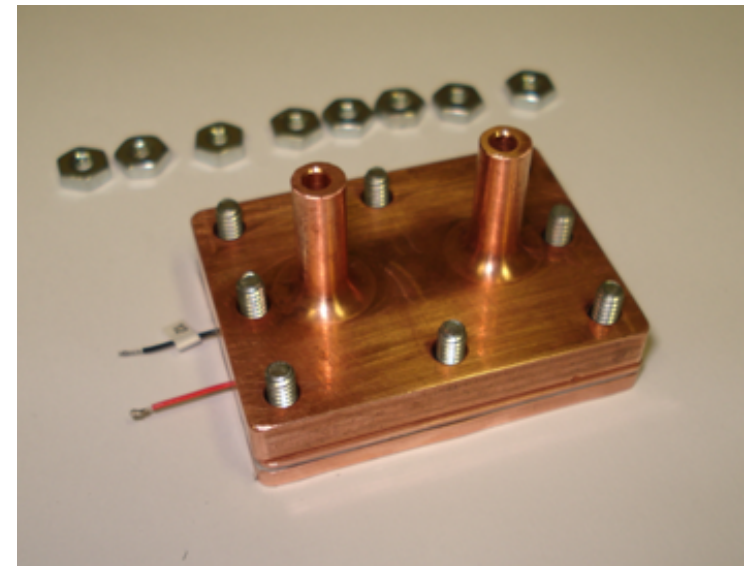
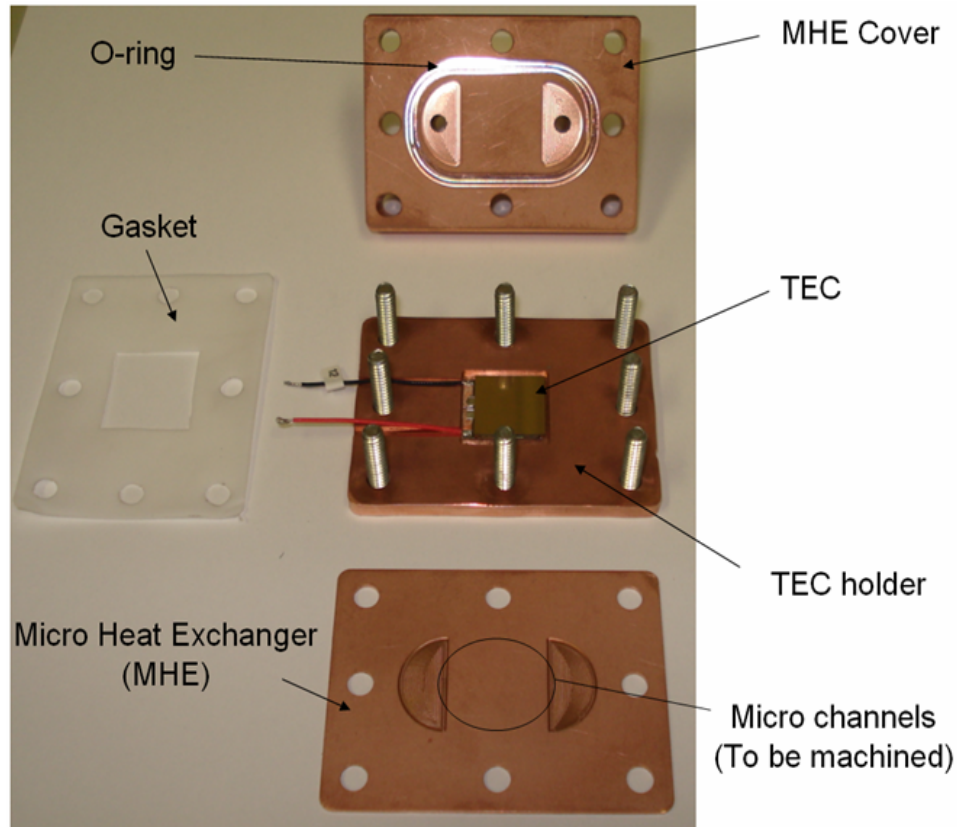
2.5 mm x 2.5 mm  
100  $\mu$ m thickness

## Embedded TEC in Package

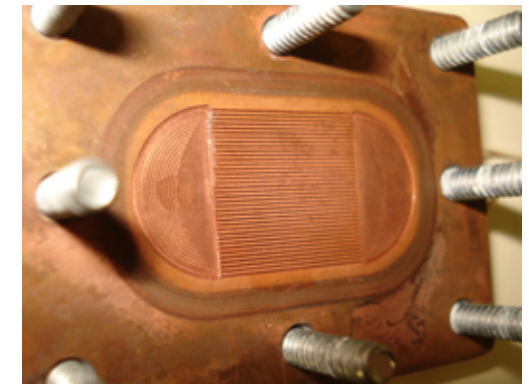
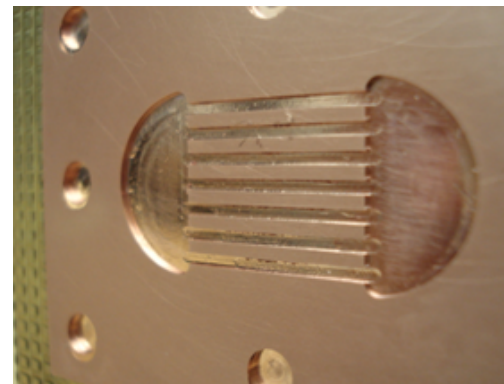
- Reduces effect of non-uniform heat transfer
- Cools hot spot by 5-15°C

# 1D Thermal Model

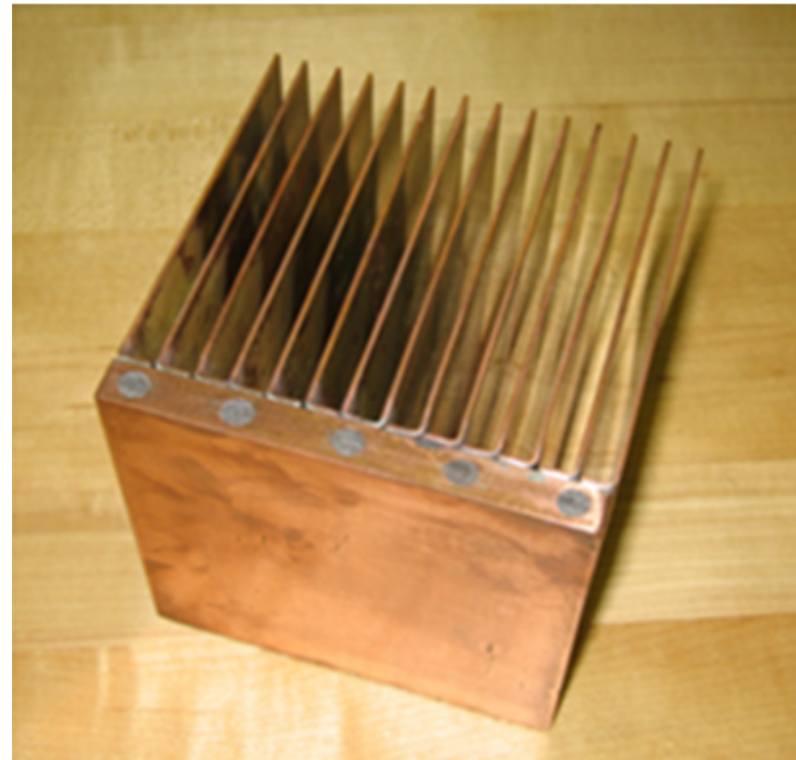
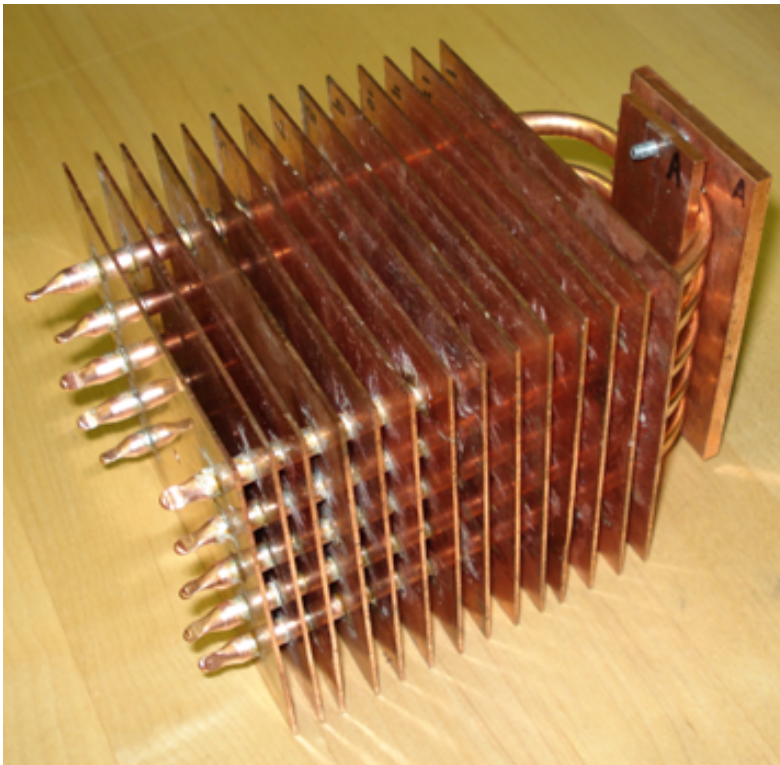




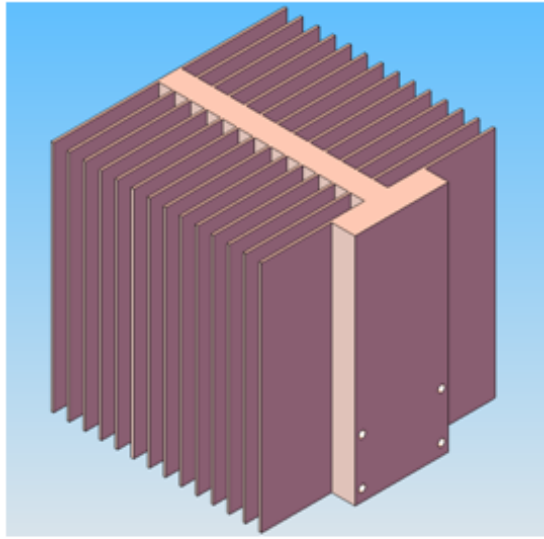
# Hybrid Systems



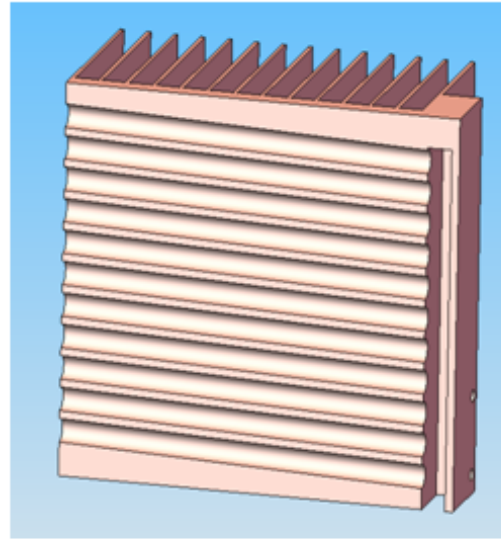
# Hybrid Systems



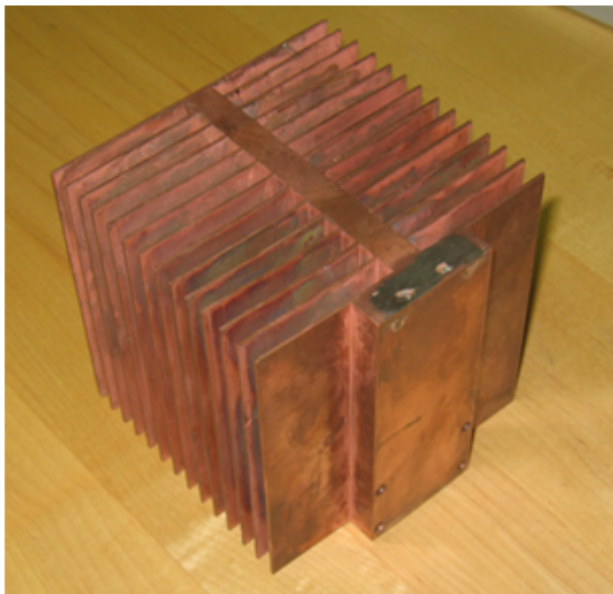




a



b



c

# Hybrid Systems

# Thermal Contact Resistance: Non-Conforming, Rough Surfaces

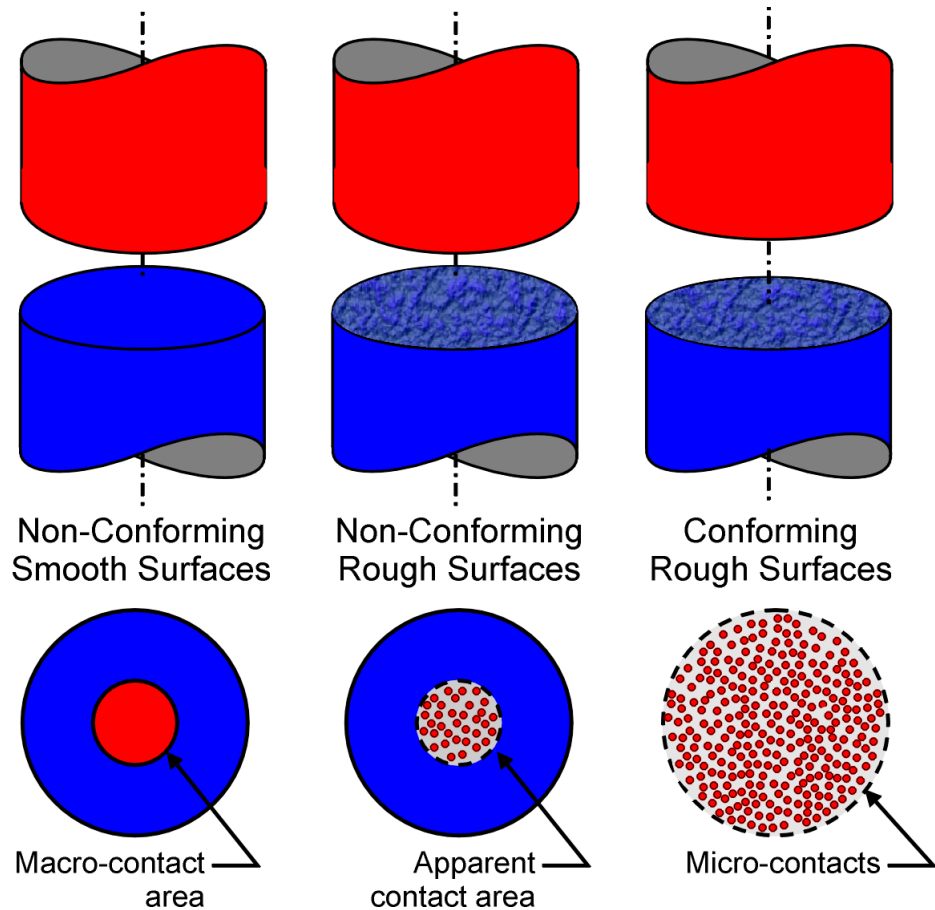


## Objectives

- develop thermo-mechanical models for predicting contact resistance in real surfaces with microscopic roughness and waviness

## Overview

- mechanical models combine the effects of plastic deformation at the microscopic level with elastic deformation at the macroscopic level

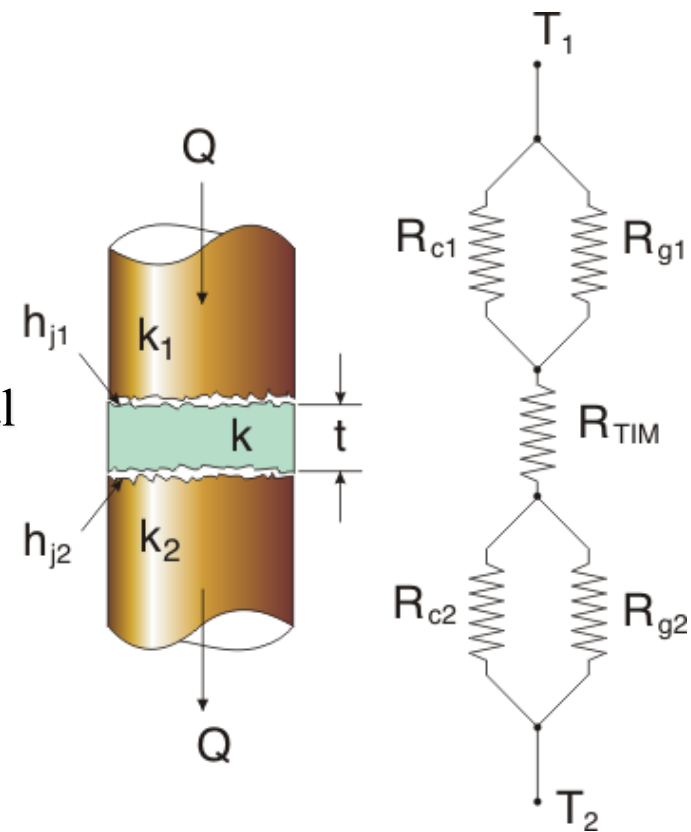




# Thermal Interface Materials



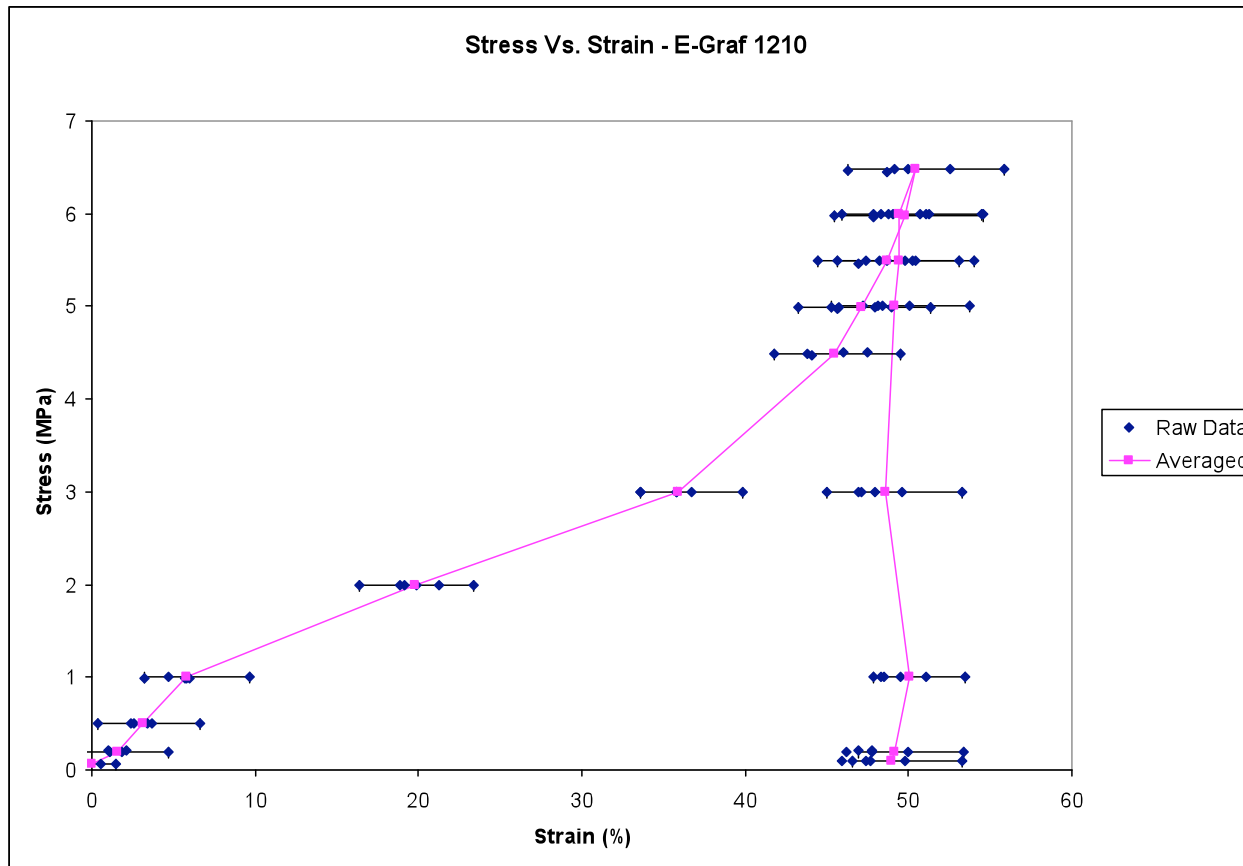
- Two major categories
  - Solid layer materials – polymers, graphite, metal foils
  - Fluidic materials – thermal grease, phase-change materials
- Current industry design practice
  - Select TIM based on manufacturer's specifications
  - Limited experimental verification or analytical modeling
- TIM manufacturer's specifications
  - Variety of measurement techniques
    - ASTM D5470 and variations
    - Laser flash diffusivity tests



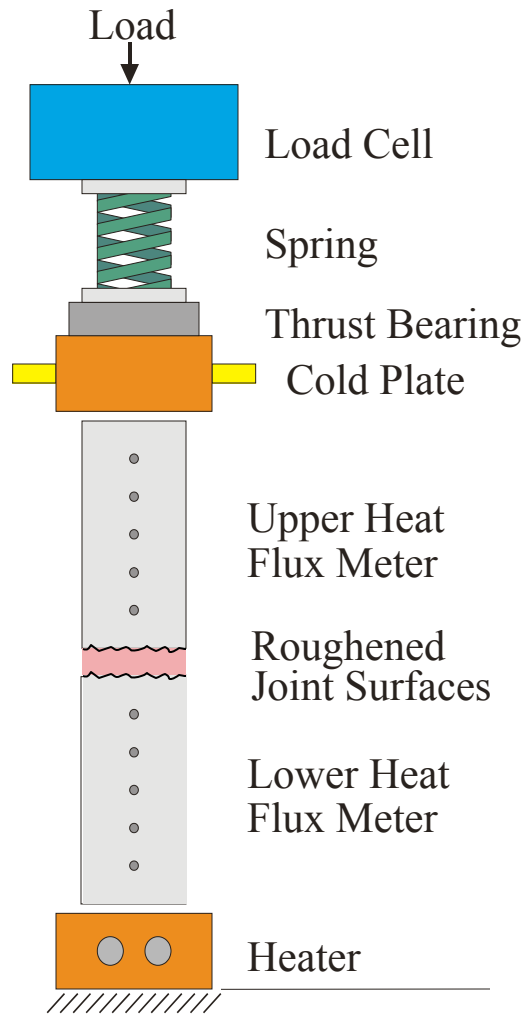
# Sample Thickness Measurements



- Thickness vs. load tests for E-Graf 1210

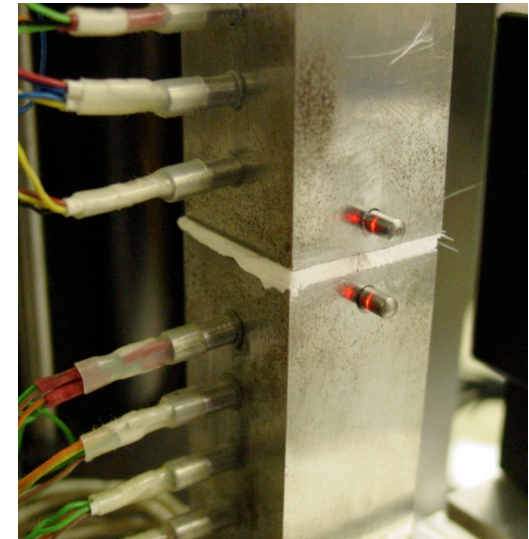
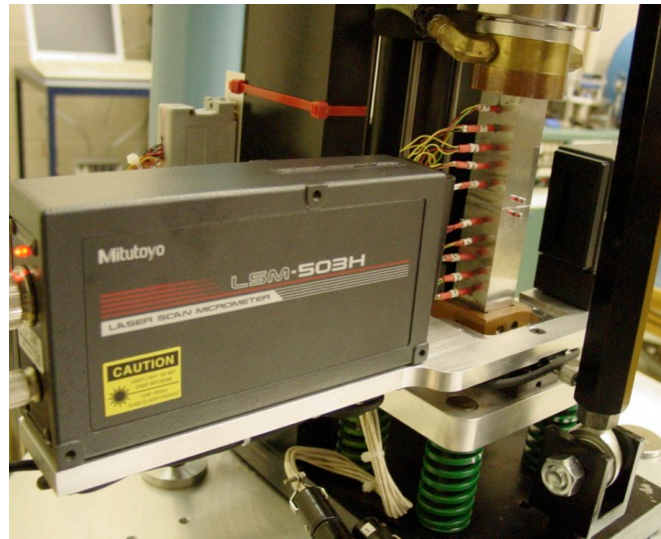


# Thermal Resistance Testing



## Thermal Interface Testing

- steady state test
  - prescribed interface pressure
  - prescribed heat load
  - measure temperature drop across the interface
  - measure heat load with flux meters
  - measure interface thickness with laser extensometer
- $$k = (Q \times t) / (A \times [T1 - T2])$$



Questions?